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APPLICATION FOR UNITED STATES LETTERS PATENT

for

**ANTENNA DIVERSITY RECEIVER**

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## **ANTENNA DIVERSITY RECEIVER**

### **FIELD OF INVENTION**

2           This invention relates to a switching system for improved FM reception. More  
specifically, a controller which selects an antenna from a plurality of antennas for  
4           superior FM reception is disclosed.

### **BACKGROUND OF INVENTION**

6           Antenna diversity receiving systems having an antenna device including a plurality  
of FM antennas are known. These systems have a controlled switching circuit for  
8           sequentially switching through one of the plurality of FM antennas via an antenna cable to  
a receiver upon reception of a switching control signal. The receiver has a multipath detector  
10          coupled to a pulse generator for generating a pulse signal at the detection of multipath  
interference. Such a receiver is described in European Patent Application number 0 792 031  
12          and is specifically suited to be used in vehicles.

          The reception of a wanted RF broadcast transmitter signal may be disturbed or  
14          otherwise deteriorated by various phenomena, such as multipath reception and/or adjacent  
channel interferences. In general, multipath reception is caused by signal reflections at and/or  
16          against environmental physical obstacles, such as mountains, trees, buildings, fences and the  
like. Due to such signal reflections an RF broadcast signal may arrive at a certain reception  
18          location through different signal paths, i.e. in different amplitude and phase conditions. The

summation of these multipath signals at the receiver antenna results in unpredictable signal  
2 amplitude and/or phase distortions, most often effectuating in part or complete cancellation  
of the useful RF reception signal. These signal cancellations, being referred to as signal dips,  
4 strongly depend on the RF carrier frequency of the received RF broadcasting signal and on  
the location of reception.

6           Signal dips severely deteriorate the desired RF broadcasting signal and also the  
overall signal reception quality. However, a relatively small shift in the position of the  
8 antenna receiving the desired RF broadcasting signal may already suffice to strongly improve  
signal reception quality. This solution is used in antenna diversity receiving systems of the  
10 above type to avoid reception of multipath distorted RF signals. In such antenna diversity  
receivers use is made of two or more antennas mutually spaced apart and coupled to an RF  
12 input of a receiver. Only the antenna having the best local receiving conditions with respect  
to the other antenna(s) is actually connected to the RF receiver input. This antenna, also  
14 referred to as the actual antenna, is effective in the reception and supply of the desired RF  
broadcasting signal through the antenna cable to the receiver as long as the multipath  
16 distortion at the actual antenna remains smaller than a certain predetermined multipath  
threshold level. As soon as the received multipath distortion exceeds the multipath threshold  
18 level, the RF signal supply to the receiver is changed from the actual antenna to another  
antenna positioned at a location with better receiving conditions. With proper control of the

controller circuit, the receiver is continuously optimized for minimum multipath reception.

2 Present antenna diversity receiving systems have a multipath detector with an output  
coupled to a pulse generator for generating a pulse signal at the detection of multipath  
4 interference. This pulse initiates a proper switching operation resulting in a switch over of  
an RF broadcast signal from one antenna to a subsequent antenna. The pulse signal is  
6 supplied through the antenna cable to the controller to initiate the antenna switching  
operation. This switching operation is repeated if the RF broadcast signal received at the  
8 subsequent antenna also appears to be affected by multipath distortion exceeding the  
multipath threshold level, until an RF broadcast signal is actually received which is not  
10 affected by such multipath distortion.

The antenna cable carries RF broadcast signals (from the antenna device to the  
12 receiver) as well as pulse signals (in the opposite direction). These signals mutually interfere  
and in particular the pulse signals effect the useful FM RF broadcast signals and may become  
14 noticeable in the reproduced audio signals.

There is thus a need to simplify existing antenna diversity receiving systems allowing  
16 for a cost effective implementation thereof, while providing optimal signal reception. There  
is also a need for an antenna diversity receiving system using a single antenna cable for the  
18 transmission of both useful FM RF broadcast signals and pulsating switching control signals  
to secure an accurate detection of these pulsating switching control signals and to prevent the

pulse signals from disturbing the processing of the useful FM RF broadcast signals in the receiver. There is a further need for a system to allow for the reception of various types of RF broadcast signals, in particular both AM and FM RF broadcast signals while preventing mutual interference between the various signals passing one and the same antenna cable, from occurring.

## **SUMMARY OF THE INVENTION**

These needs may be addressed by the present invention which is may be embodied in an antenna diversity receiving system having an antenna device including a plurality of FM antennas as well as a controllable switching circuit for sequentially switching through one of the plurality of FM antennas via an antenna cable to a receiver upon reception of a switching control signal. The receiver has a multipath detector coupled to a pulse generator for generating a pulse signal at the detection of multipath interference. The receiver also has a pulse shaper circuit following the pulse generator to convert the pulse signal of the pulse generator into a pulse signal pair. The pulse signal pair has a first signal pulse followed by a second signal pulse with a signal polarity opposite to the signal polarity of the first signal pulse. The pulse signal pair has a waveform varying symmetrically around a reference level and which is supplied through the antenna cable to the antenna device.

By applying the above components, the pulse signals passing through the antenna cable have no DC signal energy, thereby preventing any DC level variation, including DC

variations of a detection threshold level. This stabilizes the detection accuracy of the pulse signals. Furthermore, the spectral distribution of signal energy of the pulse signals prevents the pulse signals from becoming noticeable in the reproduced audio signals.

To simplify implementation of the pulse shaper, the pulse signal waveform of the pulse generator is substantially rectangular, varying during a first signal transient from a first signal level to a second signal level and during a second signal transient from said second signal level to the first signal level. The pulse shaper circuit has a signal differentiator for differentiating the pulse signal of the pulse generator to form first and second pulse spikes which have mutually opposite signal polarity. The spikes occur substantially during the first and second signal transients. The signal differentiator has a first inductance element coupled between an output resistance of the pulse generator and a DC supply voltage.

Another embodiment of the antenna diversity receiving system according to the invention is characterized by the pulse shaper circuit being coupled to the antenna cable through a first FM blocking filter which provides signal suppression within the frequency range of the FM RF broadcast frequency band. This reduces pulse signal energy within the useful FM RF broadcast frequency band at the antenna cable, and smooths the form of the pulse signal pair into a roughly, sinusoidal waveform. A cost effective implementation of the first FM blocking filter includes a first parallel LC circuit having a resonance frequency substantially corresponding to the center frequency within the frequency range of the FM RF broadcast frequency band.

Another embodiment of an antenna diversity receiving system according to the invention, providing effective detection of pulse signal pairs, includes an antenna device which has a control signal detector. The detector has an input coupled to the antenna cable for supplying pulse signal pairs from the pulse shaper circuit. The detector has an output coupled to a control input of the controllable switching circuit. The control signal detector has a threshold circuit which provides a threshold level and generates a switching control signal pulse for the controllable switching circuit when the pulse signal pair at the input of the control signal detector exceeds the threshold level. The antenna device has a counting device coupled between the control signal detector and the control input of the controllable switching circuit to simplify accurate antenna switching in consecutive order. The counting device counts the switching control signal pulses in a cycle which have a number of values corresponding to the number of fixed antennas of the antenna device.

A second FM blocking filter is provided to prevent signal leakage within the frequency range of the FM RF broadcast frequency band via the control signal path of the antenna device. The second FM filter affects signal suppression within the frequency range of the FM RF broadcast frequency band. Preferably, the second FM blocking filter has a second parallel LC circuit having a resonance frequency substantially corresponding to the center frequency within the frequency range of the FM RF broadcast frequency band.

A further preferred embodiment of an antenna diversity receiving system according to the invention, includes an antenna device having a second inductance element DC coupled

through the antenna cable in parallel to the first inductance element. The second inductance  
2 element is coupled between an input of the control signal detector and a reference voltage.  
The first and second inductance elements form part of the differentiator of the pulse shaper  
4 circuit and are given inductance values with regard to the output resistance of the pulse  
generator to properly differentiate the pulse signal of the pulse generator.

6 Another embodiment of an antenna diversity receiving system according to the  
invention includes an AM antenna coupled via an AM amplifying circuit to the antenna  
8 cable. The system includes an AM signal compensation circuit which compensates AM  
signals occurring at a first input of the AM signal compensation circuit by AM signals  
10 occurring at a second input thereof. The first and second inputs are coupled to the antenna  
cable and an output of the amplifying circuit respectively. An output of the AM signal  
12 compensation circuit is coupled to the controllable switching circuit. This measure allows  
for the reception of RF AM broadcast signals, while preventing amplitude variations due to  
14 the RF AM broadcast signals from being detected as switching control signals. False antenna  
switching operations are thus effectively avoided. Preferably, the output of the AM signal  
16 compensation circuit is coupled through the control signal detector to the controllable  
switching circuit.

18 The AM amplifying circuit is coupled through an inverter stage to the second input  
of the AM signal compensation circuit to increase the accuracy in compensation. The AM  
20 signal compensation circuit has an adder circuit for addition of the signals at the first and

second inputs of the AM signal compensation circuit. Alternatively, the AM amplifying  
circuit may have a balanced AM amplifier with non-inverting and inverting output stages of  
a balanced AM amplifier coupled to the first and the second input of the AM signal  
compensation circuit respectively

The accuracy of compensation may be further increased by a first high pass filter  
coupled between the output of the first AM signal amplifier and the antenna cable and a  
second high pass filter coupled between the output of the second AM signal amplifier and  
the second input of the AM signal compensation circuit for a high pass selection of the AM  
RF frequency band.

It is to be understood that both the foregoing general description and the following  
detailed description are not limiting but are intended to provide further explanation of the  
invention claimed. The accompanying drawings, which are incorporated in and constitute  
part of this specification, are included to illustrate and provide a further understanding of the  
method and system of the invention. Together with the description, the drawings serve to  
explain the principles of the invention.

#### **BRIEF DESCRIPTION OF THE DRAWINGS**

Figure 1 is a block diagram of an antenna diversity receiving system according to the  
invention comprising an antenna device coupled via an antenna cable to a receiver;

Figure 2 is a block diagram of a multipath detector and a pulse generator for use in

the antenna diversity receiving system of Figure 1;

2           Figure 3 is a series of time plots of the output signals of the multipath detector of  
Figure 1;

4           Figure 4 is a series of time plots of output signals of the multipath detector, the pulse  
generator and a pulse shaper following the pulse generator of Figure 1.

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**DESCRIPTION OF THE PREFERRED EMBODIMENT**

2 While the present invention is capable of embodiment in various forms, there is  
shown in the drawings and will hereinafter be described a presently preferred embodiment  
4 with the understanding that the present disclosure is to be considered as an exemplification  
of the invention, and is not intended to limit the invention to the specific embodiment  
6 illustrated.

Figure 1 shows an embodiment of an antenna diversity receiving system according  
8 to the present invention for use in cars. The system has an antenna diversity box 1, inputs  
connected to an antenna system having a single AM antenna (AM) and FM antennas (FM1-  
10 FM4). In contrast with the antennas used in the above mentioned known systems, the AM  
and FM antennas (AM and FM1-FM4), each have a fixed predetermined aerial characteristic.  
12 In a practical embodiment, the fixed predetermined aerial characteristics of the FM antennas  
FM1-FM4 are chosen to mutually differ such that they each provide a maximum aerial gain  
14 factor in mutually different directions. Preferably, the mutually differing angles of maximum  
aerial gain are chosen to cover the full angular area, in which proper reception of an RF FM  
16 broadcast signal is most likely to occur.

An output of the antenna diversity box 1 is coupled via a first antenna cable terminal  
18 2, an antenna cable 3 and a second antenna cable terminal 4 to a receiver 5. When used in a  
car, the antenna diversity box 1 is mounted close to the antenna system, e.g. an antenna  
20 structure integrated in the rear window of a car. The combination of the antenna diversity

box 1 and the antenna system may be referred to as an “antenna device.” The receiver 5 may  
be mounted elsewhere in the car, e.g. in a front dashboard panel. The antenna diversity box  
1 includes a controllable switching circuit 6 having antenna terminals s1-s4. The antenna  
terminals s1-s4 are coupled to FM antennas FM1-FM4 respectively and a switching circuit  
to connect one of the FM antennas FM1-FM4, such as the FM antenna FM4, to a switch  
output terminal s0. Upon receiving a switching control signal at a switching control input ci  
of the controllable switching circuit 6, an FM antenna is disconnected from the switch output  
terminal s0, after which another FM antenna, for example the FM antenna following in  
subsequent order after the first FM antenna, such as FM antenna FM1, is switched to be  
connected to the switch output terminal s0. The selected FM antenna supplying a broadband  
RF FM broadcast signal to the switch output terminal s0 is referred to as the actual FM  
antenna. The actual FM antenna is in a position which is somewhat shifted with regard to  
the previous actual FM antenna, and also differs in its antenna gain characteristic. This may  
improve the signal quality of the broadband RF FM broadcast signal at the switch output  
terminal s0. The switch output terminal s0 is coupled to a broadband RF FM band filter 7  
providing broadband selection and/or amplification of the received broadband RF FM signal.  
The signal is transmitted through a DC blocking capacitor Cb1 and the antenna cable  
terminal 6 to the antenna cable 3. A coaxial type cable is used for the antenna cable 3 in this  
example. The AM antenna, AM, is coupled via the antenna diversity box 1 to the first  
antenna cable terminal 2, as will be explained in more detail below.

The second antenna cable terminal 4 is an RF input for the receiver 5 and is followed  
via a DC blocking capacitor Cb2 by an AM/FM tuner 8. The broadband RF AM and FM  
signals passing the antenna cable 6 arrive at the AM/FM tuner 8, which selects and  
demodulates a desired AM RF signal into a baseband AM modulation signal and a desired  
FM RF signal into an FM IF signal followed by demodulating the FM IF signal into an FM  
stereomultiplex signal. The output signal of the AM/FM tuner 8 which is either the baseband  
AM modulation signal or the FM stereomultiplex signal, is supplied to a signal processor 9.  
The signal processor 9 processes these signals into a baseband audiosignal and into left and  
right baseband stereo signals. Reproduction of these signals takes place in first and second  
loudspeakers LS1 and LS2.

The receiver 3 also includes a multipath detector 10 coupled to the AM/FM tuner 8.  
The multipath detector 10 receives a signal from the AM/FM tuner indicative of the FM IF  
signal level, referred to as the IF level signal, as well as the FM stereomultiplex signal which  
is the tuner output signal. In this example, the multipath detector 10 is implemented with an  
type TEA 6101 integrated circuit, which is connected to a pulse generator 11. The occurrence  
of an amplitude dip in the FM IF signal coinciding with distortion in a frequency range of  
the tuner output signal above the frequency range of the FM stereomultiplex signal, is  
indicative of multipath distortion. When multipath distortion is detected, the multipath  
detector 10 triggers the pulse generator 11 to generate a pulse signal of a standard rectangular  
waveform. This waveform varies during a first signal transient from a first signal level to

a second signal level and during a second signal transient from the second signal level to the first signal level. The operation and function of the multipath detector 10 and the pulse generator 11 will be described in more detail below with reference to Figures 3 and 4.

The pulse generator 11 has an output which is coupled to a pulse shaper which includes a signal differentiating circuit RLC for differentiating the standard rectangular pulse signal waveform of the pulse generator 11. The signal differentiating circuit RLC converts the rectangular pulse signal waveform into a pulse signal pair having a first signal pulse, or a first pulse spike, followed by a second signal pulse, or a second pulse spike, having a signal polarity opposite to the signal polarity of the first signal pulse. The spike pulses occur substantially during the first and second signal transients. The overall waveform of the pulse signal pair varies symmetrically around a reference level.

The pulse shaper is coupled to a first FM blocking filter 12 providing for signal suppression within the frequency range of the FM RF broadcast frequency band. The first FM blocking filter 12 has a first parallel LC circuit having a resonance frequency substantially corresponding to the center frequency within the frequency range of the FM RF broadcast frequency band. The first FM blocking filter 12 strongly reduces the occurrence of pulse signal energy within the useful FM RF broadcast frequency band at the antenna cable, and smooths the form of the pulse signal pair. The pulse signals from the second antenna cable terminal 4, i.e. at the RF input of the receiver 5, are therefore prevented from becoming noticeable in the reproduced audio signals. Furthermore, the pulse signals passing

from the antenna cable 3 to the antenna diversity box 1, have no DC signal energy, thereby  
preventing any DC level variation, including DC variations at a detection threshold level.  
The mutually opposite polarities of the first and second signal pulses prevent any parasitic  
DC level integration at the p-n diode junctions of the transistors used in the circuitry of the  
antenna device. This stabilizes the accuracy in the detection of the pulse signals.

A bias voltage is supplied through a first inductor L1 and an inductor of the first FM  
blocking filter 12 to the second antenna cable terminal 4. The first antenna cable terminal  
2 in the antenna diversity box 1 is DC coupled through an inductor of a second FM blocking  
filter 13 to a second inductor, L2. The bias voltage is used to bias both the antenna diversity  
box 1 and the receiver 5.

The signal differentiating circuit RLC includes a resistor R coupling the output of the  
pulse generator 11 via a capacitor C to the common connection between the first inductor L1  
and the first FM blocking filter 12. The first inductor L1 is connected in parallel to the  
second inductor L2 via the inductor of the first FM blocking filter 12, the antenna cable 3,  
and the inductor of the second FM blocking filter 13. The standard rectangular pulse signal  
waveform of the pulse generator 11 is differentiated by the first and second inductors L1 and  
L2, the resistor R and the capacitor C. The resistor R may be formed by the output resistance  
of the pulse generator 11 itself. The values of the various elements (R, C, L1 and L2) are  
chosen to properly obtain the above mentioned pulse signal pair from the standard  
rectangular pulse signal waveform of the pulse generator 11.

The second FM blocking filter 13 prevents leakage of signals at the first antenna cable terminal 2 within the frequency range of the FM RF broadcast frequency band via a control signal path of the antenna device. For this purpose, the second FM blocking filter 13 is designed to effect signal suppression within the frequency range of the FM RF broadcast frequency band. Preferably, the second FM blocking filter 13 has a second parallel LC circuit having a resonance frequency substantially corresponding to the center frequency within the frequency range of the FM RF broadcast frequency band.

An output of the second FM blocking filter 13 is coupled via the first high pass filter circuit 14 and an AM signal compensation circuit 15 to a control signal detector 16 to detect the occurrence of a pulse signal pair. The control signal detector 16 has a threshold circuit providing a threshold level for effective detection of the pulse signal pairs. The control signal detector 16 generates a switching control signal pulse when the pulse signal pair occurring at the input of the control signal detector 16 exceeds the threshold level. These switching control signal pulses are indicative for the occurrence of a multipath distortion in the received RF FM signal.

The antenna device preferably has a counting device 17 coupled between the control signal detector 16 and the control input ci of said controllable switching circuit 6 to simplify accurate antenna switching in a predetermined sequential order. The output value of the counting device 17 varies monotonously with each switching control signal pulse of the control signal detector 16 within a counting cycle. The number of values within one cycle

corresponds to the number of fixed antennas FM1-FM4 of the antenna device. The use of  
the counting device 17 introduces a degree of freedom in the choice of an eventual counting  
cycle of the pulse generator 11. The counting device 17 is preferably a Johnson type counter.

The AM antenna AM is coupled via an AM amplifier 18 and the common connection  
between the second inductor L2 and the second FM blocking filter 13 to the antenna cable  
3. The second FM blocking filter 13 strongly reduces any distortion or other unwanted  
signals received by the AM antenna AM and occurring within the FM RF frequency range  
from appearing via the antenna cable 3 at the RF input of the AM/FM tuner 8.

The RF AM broadcast signals arriving at the first antenna cable terminal 2 may  
strongly vary and such amplitude variations may be mistaken for multipath indicative pulse  
signal pairs. To prevent such amplitude variations from initiating false antenna switching  
operations, the output signals of the AM amplifier 18 are connected to the second inductor  
L2 and the second FM blocking filter 13 via the first high pass band filter 14 to a first input  
of the AM signal compensation circuit 15. The output signals of the AM amplifier 18 are  
also connected to via an inverter 19 which inverts the polarity of the output signals of the  
AM amplifier 18 and a second high pass band filter 20 to a second input of the AM signal  
compensation circuit 15. The cut off frequency of the first and second high pass band filters  
14 and 20 are chosen to correspond to the lower limit frequency of the AM RF broadcast  
frequency band, i.e. 144 Khz. The first and second high pass band filters 14 and 20 select  
the broadband RF AM broadcast signals and do not hinder passage of pulse signal pairs from

the output of the second FM blocking filter 13 to the AM signal compensation circuit 15. The  
2 AM signal compensation circuit 15 provides for a cancellation of broadband AM RF signals  
supplied to its first and second inputs and may be constituted by an adder or a subtractor. In  
4 the embodiment shown signal polarity inversion performed by the inverter 19, allowing the  
use of an adder for the AM signal compensation circuit 15. Such signal polarity inversion  
6 may alternatively be obtained by using a balanced AM amplifier having non-inverting and  
inverting output stages (not shown). Another alternative is to use a subtractor for the AM  
8 signal compensation circuit 15 which removes the necessity for prior signal polarity  
inversion. The compensation of AM RF broadcast signals in the input signal path of the  
10 control signal detector 16 allows for a continuous reception of RF AM broadcast signals at  
the RF input of the AM/FM tuner 8, while preventing amplitude variations due to such RF  
12 AM broadcast signals being detected as switching control signals. False antenna switching  
operations are therefore effectively avoided.

14 The positioning of the first high pass filter 14 in the signal path between the second  
FM blocking filter 13 and the AM signal compensation circuit 15 allows for a simple DC  
16 bias provision for the AM amplifier 18.

Figure 2 shows a preferred implementation of a multipath detector 10 using a Philips'  
18 TEA6101 integrated circuit and the pulse generator 11 for use in the antenna diversity  
receiving system of Figure 1. The TEA6101 integrated circuit has 4 pin connectors fm1,  
20 fm2, fm3, and fm4. An example of the binary signals occurring at these pin connectors fm1,

fm2, fm3, fm4 upon detection of multipath distortion exceeding a certain predetermined  
multipath threshold level occurring at sequential points in time t1-t4 are shown in signal  
plots A, B, C and D respectively of Figure 3. At any point in time, only one of the binary  
signals has a high output voltage or digital "1" value. During a high output voltage or digital  
"1" value, the corresponding antenna FM1, FM2, FM3 or FM4 is switched via the antenna  
cable 3 to the RF receiver input 4. Further detailed reference of the TEA6101 integrated  
circuit may be found in the Philips IC Data Handbook which is hereby incorporated by  
reference.

The pin connectors fm2 and fm4 are coupled to exclusive OR gates G1 and G2 of the  
pulse generator 11 directly and through delay elements R1C1 and R2C2, respectively.  
Outputs of the exclusive OR gates G1 and G2 are coupled to inputs of a non-exclusive OR  
gate G3, which is connected to the pulse shaper having the differentiator circuit RLC (the  
inductor L being formed by the first and second inductors L1 and L2 in parallel). The delay  
elements R1C1 and R2C2 each are part of an RC circuit which delays the digital signal value  
supplied at the pin connectors fm2 and fm4 over an RC time constant to one of the inputs of  
the respective exclusive OR gates G1 and G2. A high or digital "1" value arising at for  
example pin connector fm2 upon detection of a multipath distortion on a point in time t1,  
will immediately be supplied to the one input of the exclusive OR gate G1 and some time  
later at the other input of said exclusive OR gate G1. This results in a pulse shaped signal  
having a rectangular waveform at the output of said exclusive OR gate G1, the pulsewidth

thereof being determined by the RC time constant of the delay element R1C1. This is further  
2 illustrated in Figure 4, in which signal plots a-c, are shown based on the signal plot B of  
Figure 3. The signal plot B in this example is the binary signal occurring at the pin connector  
4 fm2 of the multipath detector 10. The RC time constant chosen effectuates a pulsewidth of  
1.5 us. as shown in signal plot b of Figure 4. As explained above, this pulse signal is  
6 differentiated by differentiator circuit RLC which is coupled at the output of the pulse  
generator 11 resulting in a pulse signal pair having first and second spike pulses of mutually  
8 opposite polarity. The spikes formed by pulse signal pair is smoothed by the first FM  
blocking filter 12 into pulse signal pairs as shown in signal plot c of Figure 4.

10 It will be apparent to those skilled in the art that various modifications and variations  
can be made in the method and system of the present invention without departing from the  
12 spirit or scope of the invention. For example, the functions of the multipath detector 10 and  
the pulse generator 11 may be achieved with any multipath detector generating a pulse of  
14 standard rectangular waveform, each time the actually received multipath distortion increases  
above and/or decreases below a predetermined multipath threshold level. The counting  
16 device 6 may have a counting cycle different from the number of pin connectors of the IC  
TEA 6101. The pulse width may differ from the above chosen value of 1.5 us. The  
18 differentiating circuit may be implemented with an alternative frequency dependent circuit  
and/or by using a single inductance, and with a proper DC bias circuit for the AM amplifying  
20 means 18. The first high pass filter 14 may alternatively be included in the signal path

between the AM amplifying means 18 and the second FM blocking filter 13. The present  
invention is not limited by the foregoing descriptions but is intended to cover all  
modifications and variations that come within the scope of the spirit of the invention and the  
claims that follow.

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